# Modelling tanker ballast water dispersion in ports



Dr. Angus Creech acwc2@hw.ac.uk

Dr. Baixin Chen B.Chen@hw.ac.uk

Heriot-Watt University



# Introduction

- Saline ballast water (pH of 5.6) is ejected by tankers into fresh water at river ports such as Brisbane
- This is carried by the current away from the tanker
- Turbulent mixing likely
- River environment affected by the saline water, which has lower pH than river water
- Extent of ballast plume unknown

Computational fluid dynamics (CFD) can be used to model this situation.



# **Problem metrics**

- Tanker is 300m long, with a draught of 20m
- Port is 30-35m deep
- Current has max. speed of ~1 m/s
- River water has 2 ppt salinity, and density of 1000 kg/m<sup>3</sup>
- Ballast water is ejected for 18 hours at 6.12 m<sup>3</sup>/s near rear of tanker
- Ballast water has a salinity of 35 ppt



# **Model specification**



- Channel
  - Quasi-2D problem: channel ~3km x 35m (depth)
  - Vertical velocity profile at inlet (max. flow speed at top)
  - Quadratic bottom drag  $C_D = 0.043$  (roughness length 0.4m)
  - Salinity 2 ppt, density 1000 kg/m<sup>3</sup>
  - Salinity contraction coefficient 7.5 x 10<sup>-4</sup>
  - Temperature 20 ℃
- Ballast outlet
  - Flow rate 6.12 m<sup>3</sup>/s
  - Outlet boundary salinity 35ppt
  - Temperature 20 ℃



# **Model specification (2)**

NAMES OF STREET, STREE

- Simulation
  - Uses finite-element CFD to resolve flow with Boussinesq approximation to drive convection
  - Mesh resolution ~5m (at tanker) to ~8m (>1km from tanker)

(zoomed view of mesh)

- LANS turbulence modelling
- Time-step 2.5 s
- Simulation time ~ 18 hrs.
- Two simulation studies run:
  - 1) peak flow speed u=0.4 m/s
  - 2) peak flow speed u=0.8 m/s
- Normalised salinity specified as

$$\alpha = \frac{pH - pH_b}{pH_0 - pH_b}$$
 pH<sub>b</sub>: the background pH of port water  
pH<sub>0</sub>: the pH of Ballast water in the tanker



## Results :: u=0.4 m/s

### t=15 mins - coloured plot, white markers every 500m



### Contour plot, from 0.1 (white contour) to 1 in intervals of 0.05



### t=1 hour







## **Results :: u=0.4 m/s (2)**

### t=6 <sup>1</sup>/<sub>2</sub> hours – plume extent passes 2.5km downstream





### **t=14 hours** – plume has reached steady state





## **Results :: u=0.4 m/s (3)**

#### t=15 mins - zoomed to stern



#### t=14 hours - zoomed to stern





### Results :: u=0.8 m/s

### t=15 mins



### t=1 hour - plume extent ~400m greater than at u=0.4 m/s





## **Results :: u=0.8 m/s (2)**

### t=2 ¼ hours – plume extent passes 2.5km downstream



### t=9 hours - plume has reached steady state





# Results :: u=0.8 m/s (3)

t=15 mins – already the plume shape differs from the u=0.4m/s case



t=9 hours







# **Results :: comparison**

• Plume development of low and high speed flows compared





# Analysis

- Plumes extend several km downstream
- Doubling of peak flow speed shortens plume travel time:
  6 <sup>1</sup>/<sub>2</sub> hours at 0.4 m/s, to 2 <sup>1</sup>/<sub>4</sub> hours at 0.8 m/s
- **These are worst case scenarios:** 2D problem ignores lateral turbulent mixing with river water
- A 3D model would allow lateral mixing, so ballast water concentration downstream would be lower than 2D cases



# Conclusion

- 2D model can simulate saline/fresh water mixing and buoyancy plumes over large (>1 km) distances
- Shortcomings of 2D apparent in high plume concentrations downstream
- Requires three dimensional model for accurate simulation
- Future work model can be extended to include 3D flow features, including:
  - Timed operation of below-water and above-water ballast outlets
  - Lateral flow dispersal and mixing
  - Complex 3D objects such as ship hulls, quays
  - Bathymetric features, eg. variable channel depth
  - Free surfaces
  - Spatially and time-varying tidal currents